

Die Storage Rack Analysis

Cross-members: 6"x6"x1/4" HSS tubing

Long. members: 6"x6"x1/4" HSS tubing
W6"x20#

Fixed end reaction for the cross members (dist. load w lbs./in.)

$$FEA = w \cdot L / 2$$

Fixed end moment for the cross members (dist. load w lbs./in.)

$$FEM = w \cdot L^2 / 12 \quad \text{beam fixed at ends}$$

HSS tubing: $s_y = 46 \text{ ksi}$

$$\begin{aligned} L &= 96 \text{ in.} \\ w &= 250 \text{ lbs./in} \\ FEA &= 12,000 \text{ lbs.} \\ FEM &= 192,000 \text{ in-lbs.} \end{aligned}$$

$$\begin{aligned} A &= 5.24 \text{ in}^2 \\ I_x &= 28.6 \text{ in}^4 \\ S &= 9.54 \text{ in}^3 \end{aligned}$$

$$\begin{aligned} s_b &= 20,126 \text{ psi} && \text{calculated bending stress at top} \\ s_a &= 30,360 \text{ psi} && \text{allowable bending stress} \end{aligned}$$

Shear Stress:

$$\begin{aligned} Q &= 2.91 \text{ in}^3 \\ t &= 5,236 \text{ psi} && \text{calculated max. shear stress in side wall} \end{aligned}$$

$$\begin{aligned} Q &= 2.02 \text{ in}^3 \\ t &= 3,630 \text{ psi} && \text{calculated max. shear stress at corner} \end{aligned}$$

$$s_b = 18,576 \text{ psi} \quad \text{calculated bending stress at corner}$$

Combined Stress:

$$s = 19,260 \text{ psi} \quad \text{calculated stress at corner}$$

Die Storage Rack Analysis

Cross-members: 6"x6"x1/4" HSS tubing

Long. members: 6"x6"x1/4" HSS tubing
W6"x20#

I-beam: $s_y = 36$ ksi

$L = 144$ in.

$A = 5.87$ in²

$I_x = 41.4$ in⁴

$S = 13.4$ in³

Beam Forces and Moments:

$P = 12,000$ lbs. from loading on cross-member

$a = 35$ in.

$b = 109$ in.

$R_1 = 10,218$ lbs.

$R_2 = 1,782$ lbs.

Bending moment from concentrated load:

$M_1 = -240,645$ in-lbs. @ end of beam

$M_a = 116,980$ in-lbs. @ intersection of cross-member and beam

$M_c = 51,042$ in-lbs. @ center of beam

$M_b = -14,897$ in-lbs. @ intersection of cross-member and beam

$M_2 = -77,271$ in-lbs. @ end of beam

Bending moment from distributed load:

$w = 0$ lbs/in.

$M_1 = 0$ in-lbs. @ end of beam

$M_a = 0$ in-lbs. @ intersection of cross-member and beam

$M_c = 0$ in-lbs. @ center of beam

$M_b = 0$ in-lbs. @ intersection of cross-member and beam

$M_2 = 0$ in-lbs. @ end of beam

Combined Bending Moment:

$M_1 = -317,917$ in-lbs. @ end of beam

$M_a = 102,083$ in-lbs. @ intersection of cross-member and beam

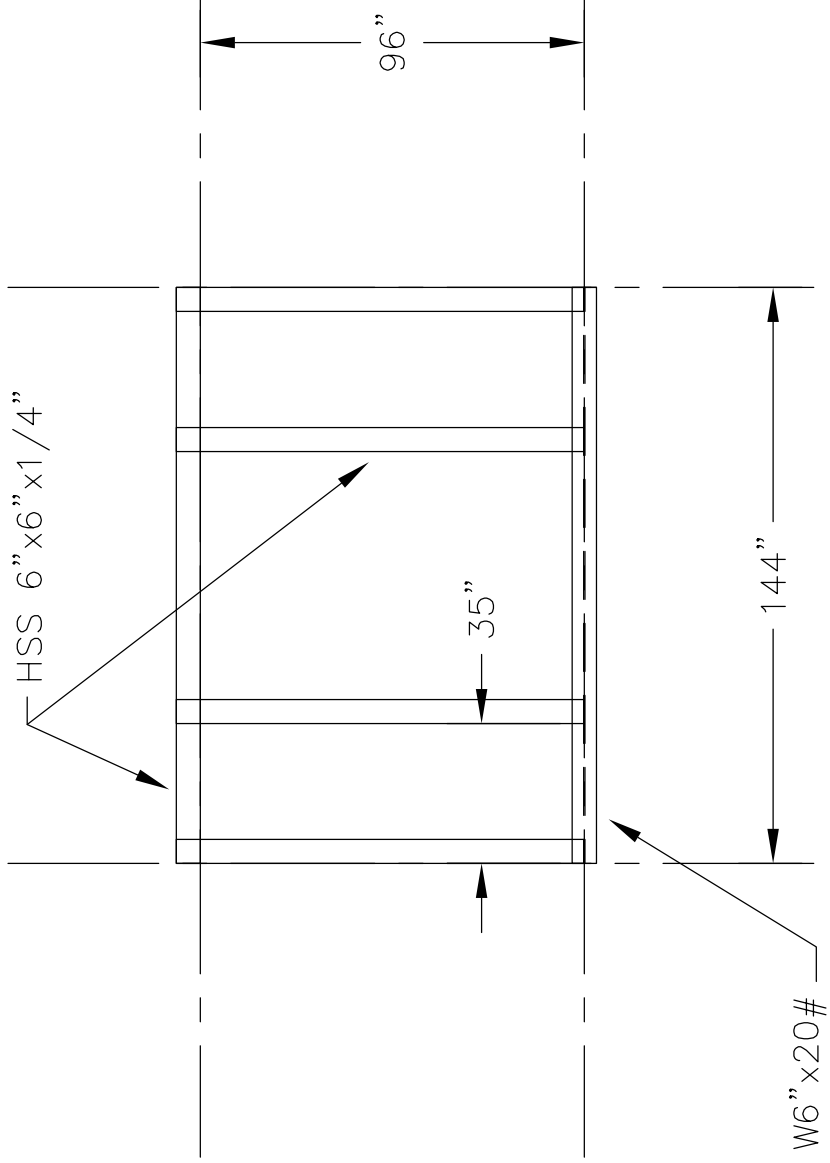
$M_c = 102,083$ in-lbs. @ center of beam

$M_b = 102,083$ in-lbs. @ intersection of cross-member and beam

$M_2 = -317,917$ in-lbs. @ end of beam

$s_b = 23,725$ psi calculated bending stress at top flange

$s_a = 23,760$ psi allowable bending stress



Reference:
The shapes contained in this database are taken from the AISC Version 13.0 "Shapes Database" CD-ROM Version (12/2005), as well as those listed in the AISC 13th Edition Manual of Steel Construction (12/2005).

NOMENCLATURE FOR AISC VERSION 13.0 MEMBER PROPERTIES AND DIMENSIONS:

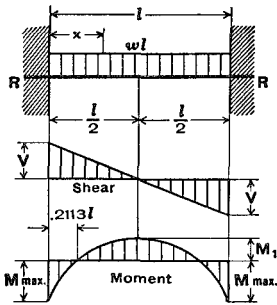
A = Cross-sectional area of member (in.^2)
 d = Depth of member, parallel to Y-axis (in.)
 h = Depth of member, parallel to Y-axis (in.)
 tw = Thickness of web of member (in.)
 bf = Width of flange of member, parallel to X-axis (in.)
 b = Width of member, parallel to X-axis (in.)
 tf = Thickness of flange of member (in.)
 k = Distance from outer face of flange to web toe of fillet (in.)
 k1 = Distance from web centerline to flange toe of fillet (in.)
 T = Distance between fillets for wide-flange or channel shape = $d(nom)-2*k(det)$ (in.) *(Note: gages for angles are available by viewing comment box at cell K18.)*
 gage = Standard gage (bolt spacing) for member (in.)
 Ix = Moment of inertia of member taken about X-axis (in.^4)
 Sx = Elastic section modulus of member taken about X-axis (in.^3)
 rx = Radius of gyration of member taken about X-axis (in.) = $\sqrt{I_x/A}$
 Iy = Moment of inertia of member taken about Y-axis (in.^4)
 Sy = Elastic section modulus of member taken about Y-axis (in.^3)
 ry = Radius of gyration of member taken about Y-axis (in.) = $\sqrt{I_y/A}$
 Zx = Plastic section modulus of member taken about X-axis (in.^3)
 Zy = Plastic section modulus of member taken about Y-axis (in.^3)
 rx = $\sqrt{I_x/(I_y*C_w)/S_x}$ (in.)
 xp = horizontal distance from designated member edge to plastic neutral axis (in.)
 yp = vertical distance from designated member edge to plastic neutral axis (in.)
 ho = Distance between centroid of flanges, d-tf (in.)
 J = Torsional moment of inertia of member (in.^4)
 Cw = Warping constant (in.^6)
 C = Torsional constant for HSS shapes (in.^3)
 a = Torsional property, $a = \sqrt{E*C_w/G*J}$ (in.)
 E = Modulus of elasticity of steel = 29,000 ksi
 G = Shear modulus of elasticity of steel = 11,200 ksi
 Wno = Normalized warping function at a point at the flange edge (in.^2)
 Sw = Warping statical moment at a point on the cross section (in.^4)
 Qt = Statical moment for a point in the flange directly above the vertical edge of the web (in.^3)
 Qw = Statical moment at the mid-depth of the section (in.^3)
 x(bar) = Distance from outside face of web of channel shape or outside face of angle leg to Y-axis (in.)
 y(bar) = Distance from outside face of outside face of flange of WT or angle leg to Y-axis (in.)
 eo = Horizontal distance from the outer edge of a channel web to its shear center (in.) = (approx.) $t^*(d-t)^2*(b-tw/2)^2/(4*k-tw/2)$
 xo = x-coordinate of shear center with respect to the centroid of the section (in.)
 yo = y-coordinate of shear center with respect to the centroid of the section (in.)
 ro(bar) = Polar radius of gyration about the shear center = $\sqrt{xo^2+yo^2+(k+ly)/A}$ (in.)
 H = Flexural constant, $H = 1-(xo^2+yo^2)/ro(bar)^2$
 LLBB = Long legs back-to-back for double angles
 SLBB = Short legs back-to-back for double angles
 h(flat) = The workable flat (straight) dimension along the height, h (in.)
 b(flat) = The workable flat (straight) dimension along the width, b (in.)
 Asurf) = The total surface area of a rectangular or square HSS section (ft.^2/ft.)
 STD = Standard weight (Schedule 40) pipe section
 XS = Extra strong (Schedule 80) pipe section
 XXS = Double-extra strong pipe section

BEAM DIAGRAMS AND FORMULAS

For various static loading conditions

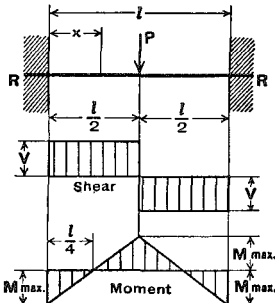
For meaning of symbols, see page 2 - 293

15. BEAM FIXED AT BOTH ENDS—UNIFORMLY DISTRIBUTED LOADS



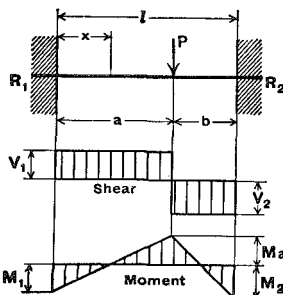
$$\begin{aligned}
 \text{Total Equiv. Uniform Load} &= \frac{2wl}{3} \\
 R = V &= \frac{wl}{2} \\
 V_x &= w\left(\frac{l}{2} - x\right) \\
 M_{\text{max. (at ends)}} &= \frac{wl^2}{12} \\
 M_1 \text{ (at center)} &= \frac{wl^2}{24} \\
 M_x &= \frac{w}{12}(6lx - l^2 - 6x^2) \\
 \Delta_{\text{max. (at center)}} &= \frac{wl^4}{384EI} \\
 \Delta_x &= \frac{wx^2}{24EI}(l - x)^2
 \end{aligned}$$

16. BEAM FIXED AT BOTH ENDS—CONCENTRATED LOAD AT CENTER



$$\begin{aligned}
 \text{Total Equiv. Uniform Load} &= P \\
 R = V &= \frac{P}{2} \\
 M_{\text{max. (at center and ends)}} &= \frac{Pl}{8} \\
 M_x \text{ (when } x < \frac{l}{2}) &= \frac{P}{8}(4x - l) \\
 \Delta_{\text{max. (at center)}} &= \frac{Pl^3}{192EI} \\
 \Delta_x \text{ (when } x < \frac{l}{2}) &= \frac{Px^2}{48EI}(3l - 4x)
 \end{aligned}$$

17. BEAM FIXED AT BOTH ENDS—CONCENTRATED LOAD AT ANY POINT



$$\begin{aligned}
 R_1 = V_1 \text{ (max. when } a < b) &= \frac{Pb^2}{l^3}(3a + b) \\
 R_2 = V_2 \text{ (max. when } a > b) &= \frac{Pa^2}{l^3}(a + 3b) \\
 M_1 \text{ (max. when } a < b) &= \frac{Pab^2}{l^2} \\
 M_2 \text{ (max. when } a > b) &= \frac{Pa^2b}{l^2} \\
 M_a \text{ (at point of load)} &= \frac{2Pa^2b^2}{l^3} \\
 M_x \text{ (when } x < a) &= R_1x - \frac{Pab^2}{l^2} \\
 \Delta_{\text{max. (when } a > b \text{ at } x = \frac{2al}{3a+b})} &= \frac{2Pa^3b^2}{3EI(3a+b)^2} \\
 \Delta_a \text{ (at point of load)} &= \frac{Pa^3b^3}{3EI l^3} \\
 \Delta_x \text{ (when } x < a) &= \frac{Pb^2x^2}{6EI l^3}(3al - 3ax - bx)
 \end{aligned}$$